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Edition

# Modern Control Systems

Twelfth Edition

Richard C. Dorf  
Robert H. Bishop

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# *Modern Control Systems*

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**TWELFTH EDITION**

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University of California, Davis

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**PEARSON**

Boston Columbus Indianapolis New York San Francisco Upper Saddle River  
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# Contents

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*Preface 11*

*About the Authors 22*

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## **CHAPTER 1** *Introduction to Control Systems 23*

---

- 1.1 Introduction 24
- 1.2 Brief History of Automatic Control 27
- 1.3 Examples of Control Systems 32
- 1.4 Engineering Design 39
- 1.5 Control System Design 40
- 1.6 Mechatronic Systems 43
- 1.7 Green Engineering 47
- 1.8 The Future Evolution of Control Systems 49
- 1.9 Design Examples 50
- 1.10 Sequential Design Example: Disk Drive Read System 54
- 1.11 Summary 56
  - Skills Check 57 • Exercises 59 • Problems 61 • Advanced Problems 66 • Design Problems 68 • Terms and Concepts 70

---

## **CHAPTER 2** *Mathematical Models of Systems 71*

---

- 2.1 Introduction 72
- 2.2 Differential Equations of Physical Systems 72
- 2.3 Linear Approximations of Physical Systems 77
- 2.4 The Laplace Transform 80
- 2.5 The Transfer Function of Linear Systems 87
- 2.6 Block Diagram Models 101
- 2.7 Signal-Flow Graph Models 106
- 2.8 Design Examples 112
- 2.9 The Simulation of Systems Using Control Design Software 135
- 2.10 Sequential Design Example: Disk Drive Read System 150
- 2.11 Summary 152
  - Skills Check 153 • Exercises 157 • Problems 163 • Advanced Problems 175 • Design Problems 177 • Computer Problems 179 • Terms and Concepts 181

---

## **CHAPTER 3** *State Variable Models 183*

---

- 3.1 Introduction 184
- 3.2 The State Variables of a Dynamic System 184

- 3.3 The State Differential Equation 188
- 3.4 Signal-Flow Graph and Block Diagram Models 193
- 3.5 Alternative Signal-Flow Graph and Block Diagram Models 204
- 3.6 The Transfer Function from the State Equation 209
- 3.7 The Time Response and the State Transition Matrix 211
- 3.8 Design Examples 215
- 3.9 Analysis of State Variable Models Using Control Design Software 228
- 3.10 Sequential Design Example: Disk Drive Read System 231
- 3.11 Summary 235  
 Skills Check 236 • Exercises 239 • Problems 242 • Advanced  
 Problems 249 • Design Problems 252 • Computer Problems 253 •  
 Terms and Concepts 254

## **CHAPTER 4**    *Feedback Control System Characteristics*    256

---

- 4.1 Introduction 257
- 4.2 Error Signal Analysis 259
- 4.3 Sensitivity of Control Systems to Parameter Variations 261
- 4.4 Disturbance Signals in a Feedback Control System 264
- 4.5 Control of the Transient Response 269
- 4.6 Steady-State Error 272
- 4.7 The Cost of Feedback 275
- 4.8 Design Examples 276
- 4.9 Control System Characteristics Using Control Design  
 Software 290
- 4.10 Sequential Design Example: Disk Drive Read System 295
- 4.11 Summary 299  
 Skills Check 301 • Exercises 305 • Problems 309 • Advanced  
 Problems 315 • Design Problems 318 • Computer Problems 322 •  
 Terms and Concepts 325

## **CHAPTER 5**    *The Performance of Feedback Control Systems*    326

---

- 5.1 Introduction 327
- 5.2 Test Input Signals 327
- 5.3 Performance of Second-Order Systems 330
- 5.4 Effects of a Third Pole and a Zero on the Second-Order System  
 Response 336
- 5.5 The  $s$ -Plane Root Location and the Transient Response 342
- 5.6 The Steady-State Error of Feedback Control Systems 344
- 5.7 Performance Indices 352
- 5.8 The Simplification of Linear Systems 361
- 5.9 Design Examples 364
- 5.10 System Performance Using Control Design Software 378
- 5.11 Sequential Design Example: Disk Drive Read System 382

- 5.12 Summary 386  
Skills Check 386 • Exercises 390 • Problems 393 • Advanced  
Problems 399 • Design Problems 401 • Computer Problems 404 •  
Terms and Concepts 406

---

## CHAPTER 6 *The Stability of Linear Feedback Systems* 408

---

- 6.1 The Concept of Stability 409  
6.2 The Routh–Hurwitz Stability Criterion 413  
6.3 The Relative Stability of Feedback Control Systems 421  
6.4 The Stability of State Variable Systems 423  
6.5 Design Examples 426  
6.6 System Stability Using Control Design Software 435  
6.7 Sequential Design Example: Disk Drive Read System 443  
6.8 Summary 446  
Skills Check 447 • Exercises 450 • Problems 452 • Advanced  
Problems 457 • Design Problems 460 • Computer Problems 462 •  
Terms and Concepts 464

---

## CHAPTER 7 *The Root Locus Method* 465

---

- 7.1 Introduction 466  
7.2 The Root Locus Concept 466  
7.3 The Root Locus Procedure 471  
7.4 Parameter Design by the Root Locus Method 489  
7.5 Sensitivity and the Root Locus 495  
7.6 PID Controllers 502  
7.7 Negative Gain Root Locus 514  
7.8 Design Examples 518  
7.9 The Root Locus Using Control Design Software 532  
7.10 Sequential Design Example: Disk Drive Read System 538  
7.11 Summary 540  
Skills Check 544 • Exercises 548 • Problems 552 • Advanced  
Problems 561 • Design Problems 565 • Computer Problems 571 •  
Terms and Concepts 573

---

## CHAPTER 8 *Frequency Response Methods* 575

---

- 8.1 Introduction 576  
8.2 Frequency Response Plots 578  
8.3 Frequency Response Measurements 599  
8.4 Performance Specifications in the Frequency Domain 601  
8.5 Log Magnitude and Phase Diagrams 604  
8.6 Design Examples 605

- 8.7 Frequency Response Methods Using Control Design Software 618
- 8.8 Sequential Design Example: Disk Drive Read System 624
- 8.9 Summary 625  
 Skills Check 630 • Exercises 635 • Problems 638 • Advanced  
 Problems 648 • Design Problems 650 • Computer Problems 653 •  
 Terms and Concepts 655

---

## CHAPTER 9 *Stability in the Frequency Domain* 656

---

- 9.1 Introduction 657
- 9.2 Mapping Contours in the  $s$ -Plane 658
- 9.3 The Nyquist Criterion 664
- 9.4 Relative Stability and the Nyquist Criterion 675
- 9.5 Time-Domain Performance Criteria in the Frequency Domain 683
- 9.6 System Bandwidth 690
- 9.7 The Stability of Control Systems with Time Delays 690
- 9.8 Design Examples 695
- 9.9 PID Controllers in the Frequency Domain 713
- 9.10 Stability in the Frequency Domain Using Control Design Software 714
- 9.11 Sequential Design Example: Disk Drive Read System 722
- 9.12 Summary 725  
 Skills Check 733 • Exercises 737 • Problems 743 • Advanced  
 Problems 753 • Design Problems 757 • Computer Problems 762 •  
 Terms and Concepts 764

---

## CHAPTER 10 *The Design of Feedback Control Systems* 765

---

- 10.1 Introduction 766
- 10.2 Approaches to System Design 767
- 10.3 Cascade Compensation Networks 769
- 10.4 Phase-Lead Design Using the Bode Diagram 773
- 10.5 Phase-Lead Design Using the Root Locus 779
- 10.6 System Design Using Integration Networks 786
- 10.7 Phase-Lag Design Using the Root Locus 789
- 10.8 Phase-Lag Design Using the Bode Diagram 794
- 10.9 Design on the Bode Diagram Using Analytical Methods 798
- 10.10 Systems with a Prefilter 800
- 10.11 Design for Deadbeat Response 803
- 10.12 Design Examples 805
- 10.13 System Design Using Control Design Software 818
- 10.14 Sequential Design Example: Disk Drive Read System 824
- 10.15 Summary 826  
 Skills Check 828 • Exercises 832 • Problems 836 • Advanced  
 Problems 845 • Design Problems 848 • Computer Problems 853 •  
 Terms and Concepts 855

## CHAPTER 11 *The Design of State Variable Feedback Systems* 856

---

- 11.1 Introduction 857
- 11.2 Controllability and Observability 857
- 11.3 Full-State Feedback Control Design 863
- 11.4 Observer Design 869
- 11.5 Integrated Full-State Feedback and Observer 873
- 11.6 Reference Inputs 879
- 11.7 Optimal Control Systems 881
- 11.8 Internal Model Design 891
- 11.9 Design Examples 895
- 11.10 State Variable Design Using Control Design Software 904
- 11.11 Sequential Design Example: Disk Drive Read System 910
- 11.12 Summary 912
  - Skills Check 912 • Exercises 916 • Problems 918 • Advanced Problems 922 • Design Problems 925 • Computer Problems 928 • Terms and Concepts 930

## CHAPTER 12 *Robust Control Systems* 932

---

- 12.1 Introduction 933
- 12.2 Robust Control Systems and System Sensitivity 934
- 12.3 Analysis of Robustness 938
- 12.4 Systems with Uncertain Parameters 940
- 12.5 The Design of Robust Control Systems 942
- 12.6 The Design of Robust PID-Controlled Systems 948
- 12.7 The Robust Internal Model Control System 954
- 12.8 Design Examples 957
- 12.9 The Pseudo-Quantitative Feedback System 974
- 12.10 Robust Control Systems Using Control Design Software 975
- 12.11 Sequential Design Example: Disk Drive Read System 980
- 12.12 Summary 982
  - Skills Check 983 • Exercises 987 • Problems 989 • Advanced Problems 993 • Design Problems 996 • Computer Problems 1002 • Terms and Concepts 1004

## CHAPTER 13 *Digital Control Systems* 1006

---

- 13.1 Introduction 1007
- 13.2 Digital Computer Control System Applications 1007
- 13.3 Sampled-Data Systems 1009
- 13.4 The  $z$ -Transform 1012
- 13.5 Closed-Loop Feedback Sampled-Data Systems 1017

- 13.6 Performance of a Sampled-Data, Second-Order System 1021
- 13.7 Closed-Loop Systems with Digital Computer Compensation 1023
- 13.8 The Root Locus of Digital Control Systems 1026
- 13.9 Implementation of Digital Controllers 1030
- 13.10 Design Examples 1031
- 13.11 Digital Control Systems Using Control Design Software 1040
- 13.12 Sequential Design Example: Disk Drive Read System 1045
- 13.13 Summary 1047
  - Skills Check 1047 • Exercises 1051 • Problems 1053 •
  - Advanced Problems 1055 • Design Problems 1056 • Computer
  - Problems 1058 • Terms and Concepts 1059

**APPENDIX A** *MATLAB Basics* 1060

*References* 1078

*Index* 1093

 **WEB RESOURCES**

**APPENDIX B** *MathScript RT Module Basics*

**APPENDIX C** *Symbols, Units, and Conversion Factors*

**APPENDIX D** *Laplace Transform Pairs*

**APPENDIX E** *An Introduction to Matrix Algebra*

**APPENDIX F** *Decibel Conversion*

**APPENDIX G** *Complex Numbers*

**APPENDIX H** *z-Transform Pairs Preface*

**APPENDIX I** *Discrete-Time Evaluation of the Time Response*



# Index

- Absolute stability.** A system description that reveals whether a system is stable or not stable without consideration of other system attributes such as degree of stability. 409, 464
- Acceleration error constant,  $K_a$ .** The constant evaluated as  $\lim_{s \rightarrow 0} [s^2 G_c(s)G(s)]$ . The steady-state error for a parabolic input,  $r(t) = At^2/2$ , is equal to  $A/K_a$ . 347, 406
- Acceleration input, steady-state error. 346–347
- Accelerometer. 101, 113, 128–131
- Ackermann's formula. 856, 867–868, 872, 877–878, 909–911, 920
- Across-variable.** A variable determined by measuring the difference of the values at the two ends of an element, 73, 75
- Actuator.** The device that causes the process to provide the output. The device that provides the motive power to the process, 92, 181
- Additive perturbation.** A system perturbation model expressed in the additive form  $G_d(s) = G(s) + A(s)$ , where  $G(s)$  is the nominal process function,  $A(s)$  is the perturbation that is bounded in magnitude, and  $G_d(s)$  is the family of perturbed process functions, 938, 1004
- Agricultural systems. 37
- Aircraft, and computer-aided design, 42
- unmanned, 38
- Aircraft attitude control. 368–378
- Aircraft autopilot. 957
- Airplane control. 314, 554, 561–562, 848–849
- All-pass network.** A nonminimum-phase system that passes all frequencies with equal gain, 595–596, 655
- Alternative signal-flow graph, and block diagram models. 204–209
- Ambler. 610
- Amplidyne. 165
- Amplifier, feedback. 263–264
- Amplitude quantization error.** The sampled signal available only with a limited precision. The error between the actual signal and the sampled signal, 1011–1012, 1059
- Analogous variables.** Variables associated with electrical, mechanical, thermal, and fluid systems possessing similar solutions providing the analyst with the ability to extend the solution of one system to all analogous systems with the same describing differential equations, 77
- Analog-to-digital converter, 1007, 1011
- Analysis of robustness. 938–940
- Anesthesia, blood pressure control during. 281–289
- Angle of departure.** The angle at which a locus leaves a complex pole in the  $s$ -plane. 480–481, 484, 499–501, 573
- Angle of the asymptotes.** The angle that the asymptote makes with respect to the real axis,  $\phi_A$ . 473, 476, 573
- Antiskid braking systems. 995
- Arc welding. 453
- Armature-controlled motor. 94, 95, 99, 111, 127, 150, 175, 177
- Array operations in MATLAB, 1067–1068
- Artificial hand. 34, 37, 66
- Assumptions.** Statements that reflect situations and conditions that are taken for granted and without proof. In control systems, assumptions are often employed to simplify the physical dynamical models of systems under consideration to make the control design problem more tractable. 72, 116–117, 181
- Asymptote.** The path the root locus follows as the parameter becomes very large and approaches infinity. The number of asymptotes is equal to the number of poles minus the number of zeros. 473, 573
- of root locus. 473
- Asymptote centroid.** The center of the linear asymptotes,  $\sigma_A$ . 474, 573
- Asymptotic approximation for a Bode diagram. 584
- Automated guided vehicle (AGV). 842
- Automatic control, history of. 27–31
- Automatic fluid dispenser. 251
- Automatic test system. 895–897
- Automation.** The control of a process by automatic means. 29, 70
- Automobile steering control system. 32
- Automobile velocity control. 527–532
- Automobiles, hybrid fuel vehicles. 44, 70
- Auxiliary polynomial.** The equation that immediately precedes the zero entry in the Routh array, 418, 464
- Avemar ferry hydrofoil. 837–838
- Axis shift. 422
- Backward difference rule.** A computational method of approximating the time derivative of a function given by  $\dot{x}(kT) = \frac{x(kT) - x((k-1)T)}{T}$ , where  $t = kT$ ,  $T$  is the sample time, and  $k = 1, 2, \dots$ . 1030, 1059
- Bandwidth.** The frequency at which the frequency response has declined 3 dB from its low-frequency value. 602, 655, 685, 764

- Bellman, R., 30
- Biological control system, 37
- Black, H. S., 28, 31, 168, 934
- Block diagram.** Unidirectional, operational blocks that represent the transfer functions of the elements of the system, 101, 102, 181
- Block diagram models, 101–106, 142–149
- alternative signal-flow graphs, 204–209
- signal-flow graphs, 193–204
- Block diagram transformations, 103–104
- Blood pressure control and anesthesia, 281–289
- Bobbin drive, 960–962
- Bode, H. W., 582, 934
- Bode plot.** The logarithm of magnitude of the transfer function is plotted versus the logarithm of  $\omega$ , the frequency. The phase,  $\phi$ , of the transfer function is separately plotted versus the logarithm of the frequency, 582–583, 625, 655, 656
- asymptotic approximation, 584
- Boring machine system, 276–279
- Bounded response, 409
- Branch.** A unidirectional path segment in a signal-flow graph that relates the dependency of an input and an output variable, 106
- Break frequency.** The frequency at which the asymptotic approximation of the frequency response for a pole (or zero) changes slope, 584, 587, 655
- Breakaway point.** The point on the real axis where the locus departs from the real axis of the  $s$ -plane, 476–478, 573
- Bridge, Tacoma Narrows, 410–412
- Camera control, 357–361, 393
- Canonical form.** A fundamental or basic form of the state variable model representation, including phase variable canonical form, input feedforward canonical form, diagonal canonical form, and Jordan canonical form, 195, 254
- Capek, Karel, 34
- Cascade compensation network.** A compensator network placed in cascade or series with the system process, 767, 769–773, 855
- Cauchy's theorem.** If a contour encircles  $Z$  zeros and  $P$  poles of  $F(s)$  traversing clockwise, the corresponding contour in the  $F(s)$ -plane encircles the origin of the  $F(s)$ -plane  $N = Z - P$  times clockwise, 657, 660–664, 764
- Characteristic equation.** The relation formed by equating to zero the denominator of a transfer function, 82, 181, 440
- Circles, constant, 685
- Closed-loop feedback control system.** A system that uses a measurement of the output and compares it with the desired output to control the process, 25, 70
- Closed-loop feedback sampled-data system, 1017–1021
- Closed-loop frequency response.** The frequency response of the closed-loop transfer function  $T(j\omega)$ , 685, 764
- Closed-loop system.** A system with a measurement of the output signal and a comparison with the desired output to generate an error signal that is applied to the actuator, 258, 325
- Closed-loop transfer function.** A ratio of the output signal to the input signal for an interconnection of systems when all the feedback or feedforward loops have been closed or otherwise accounted for. Generally obtained by block diagram or signal-flow graph reduction, 104, 115, 181, 439–440
- Command following.** An important aspect of control system design wherein a nonzero reference input is tracked, 879, 930
- Compensation.** The alteration or adjustment of a control system in order to provide a suitable performance, 766, 855
- of controls systems, 818
- using a phase-lag network on the Bode diagram, 789
- using a phase-lag network on the  $s$ -plane, 790
- using a phase-lead network on the Bode diagram, 773
- using a phase-lead network on the  $s$ -plane, 779
- using analytical methods, 798
- using integration networks, 786
- using state-variable feedback, 856
- Compensator.** An additional component or circuit that is inserted into the system to compensate for a performance deficiency, 557, 766, 855, 857
- Compensator design, full-state feedback and observer, 873
- Complementary sensitivity function.** The function  $T(s) = \frac{G_c(s)G(s)}{1 + G_c(s)G(s)}$  that satisfies the relationship  $S(s) + T(s) = 1$ , where  $S(s)$  is the sensitivity function. The function  $T(s)$  is the closed-loop transfer function, 260, 938, 1004
- Complexity.** A measure of the structure, intricateness, or behavior of a system that characterizes the relationships and interactions between various components, 39, 325
- in cost of feedback, 275–276
- Complexity of design.** The intricate pattern of interwoven parts and knowledge required, 39, 70
- Components.** The parts, subsystems, or subassemblies that comprise a total system, 325
- in cost of feedback, 275
- Computer control systems, 1006, 1007
- for electric power plant, 36
- Computer-aided design, 42
- Computer-aided engineering (CAE), 44
- Conditionally stable system, 556
- Conformal mapping.** A contour mapping that retains the angles on the  $s$ -plane on the  $F(s)$ -plane, 659, 764
- Congress, 38
- Constant  $M$  circles, 686
- Constant  $N$  circles, 686
- Continuous design problem (CDP), 68, 177, 252, 318, 401, 460, 565, 650, 757, 848, 925, 996, 1056
- Contour map.** A contour or trajectory in one plane is mapped into another plane by a relation  $F(s)$ , 658, 764
- Contours in the  $s$ -plane, 658–664
- Control engineering, 24, 29–30, 32

- Control system.** An interconnection of components forming a system configuration that will provide a desired response. 24, 70, 257  
 characteristics using m-files. 291  
 design, 40-43  
 modern examples, 32-39
- Controllability.** 857-863
- Controllability matrix.** A linear system is (completely) controllable if and only if the controllability matrix  $P_c = [B \ AB \ A^2B \ \dots \ A^{n-1}B]$  has full rank, where  $A$  is an  $n \times n$  matrix. For single-input, single-output linear systems, the system is controllable if and only if the determinant of the  $n \times n$  controllability matrix  $P_c$  is nonzero, 858, 930
- Controllable system.** A system is controllable on the interval  $[t_0, t_f]$  if there exists a continuous input  $u(t)$  such that any initial state  $x(t_0)$  can be driven to any arbitrary final state  $x(t_f)$ , in a finite time interval  $t_f - t_0 > 0$ . 858, 930
- conv function.** 138, 1075
- Convolution signal.** 329
- Corner frequency.** See Break frequency
- Cost of feedback.** 275-276
- Coulomb damper.** A type of mechanical damper where the model of the friction force is a nonlinear function of the mass velocity and possesses a discontinuity around zero velocity. Also known as dry friction, 75
- Critical damping.** The case where damping is on the boundary between underdamped and overdamped, 84, 136, 181
- Critically damped system.** 136
- Damped oscillation.** An oscillation in which the amplitude decreases with time, 86, 181
- Dampers.** 75
- Damping ratio.** A measure of damping. A dimensionless number for the second-order characteristic equation, 84, 181, 330, 332, 334-335  
 estimation of, 334
- DC amplifier.** 100
- DC motor.** An electric actuator that uses an input voltage as a control variable, 92  
 armature controlled, 94, 111, 181  
 field controlled, 93
- Deadbeat response.** A system with a rapid response, minimal overshoot, and zero steady-state error for a step input, 803, 855
- Decade.** A factor of 10 in frequency (e.g., the range of frequencies from 1 rad/s to 10 rad/s is one decade), 584, 655  
 of frequencies, 584
- Decibel (dB).** The units of the logarithmic gain, 583, 655
- Decoupled state variable model.** 205
- Design.** The process of conceiving or inventing the forms, parts, and details of a system to achieve a reasoned purpose, 39-40, 70
- Design gap.** A gap between the complex physical system and the design model intrinsic to the progression from the initial concept to the final product, 39, 70
- Design of a control system.** The arrangement or the plan of the system structure and the selection of suitable components and parameters, 766, 855  
 robot control, 453  
 in time domain, 857  
 using a phase-lag network on the Bode diagram, 794  
 using a phase-lag network on the  $s$ -plane, 789, 790  
 using a phase-lead network on the Bode diagram, 773  
 using a phase-lead network on the  $s$ -plane, 779  
 using integration networks, 786  
 using state-feedback, 856
- Design specifications.** A set of prescribed performance criteria, 327, 406
- Detectable.** A system in which the states that are unobservable are naturally stable, 861, 930
- Dexterous Hand Master (DHM).** 996
- Diagonal canonical form.** A decoupled canonical form displaying the  $n$  distinct system poles on the diagonal of the state variable representation  $A$  matrix, 205, 254
- Diesel electric locomotive control.** 898-904
- Differential equations.** An equation including differentials of a function, 72, 89, 181
- Differential operator.** 82
- Differentiating circuit.** 98
- Digital audio tape controller.** 965-974
- Digital computer compensator.** A system that uses a digital computer as the compensator element, 1023-1026, 1059
- Digital control system.** A control system using digital signals and a digital computer to control a process, 1006-1059
- Digital control systems using control design software.** 1040-1045
- Digital controllers, implementation of.** 1030-1031
- Digital-to-analog converter.** 1010
- Direct-drive arm.** 743
- Discrete-time approximation.** 239
- Disk drive read system.** See Sequential design example
- Disturbance.** An unwanted input signal that affects the output signal, 25, 70
- Disturbance rejection property.** 265-268
- Disturbance signal.** An unwanted input signal that affects the system's output signal, 264-269, 325
- Dominant roots.** The roots of the characteristic equation that represent or dominate the closed-loop transient response, 337, 406, 485, 473, 603, 655
- Drebbel, Cornelis.** 27
- Dynamics of physical systems.** 71
- Electric power industry.** 35, 36
- Electric traction motor.** 113, 126-128, 136, 148
- Electric ventricular assist device (EVAD).** 756-757
- Electrohydraulic actuator.** 95, 96, 166-167
- Electrohydraulic servomechanisms.** 744

- Embedded control.** Feedback control system that employs on-board special-purpose digital computers as integral components of the feedback loop. 46
- Energy storage systems (green engineering). 48
- Engineering design.** The process of designing a technical system. 39–40, 70
- English channel tunnel boring system. 276–279, 292–295
- Engraving machine. 605, 607–610, 621–623
- Environmental monitoring (green engineering). 48
- Epidemic disease, model of. 206–207, 425–426
- Equilibrium state. 207
- Error, steady-state. 272–275
- Error constants  
acceleration input. 346  
position. 345  
ramp. 346  
velocity. 346
- Error signal.** The difference between the desired output  $R(s)$  and the actual output  $Y(s)$ . Therefore,  $E(s) = R(s) - Y(s)$ , 143, 181, 237, 259, 325  
analysis. 259–260
- Error-squared performance indices. 882
- Estimation error.** The difference between the actual state and the estimated state  $\mathbf{e}(t) = \mathbf{x}(t) - \hat{\mathbf{x}}(t)$ . 869, 930
- Evans, R., 466
- Examples of control systems. 32–39
- Exponential matrix function. 189
- Extender. 172–173, 248, 843–844
- Federal Reserve Board. 37
- Feedback. 25  
amplifier. 263–264  
control system. 25, 32–34, 818–824  
cost of. 275–276  
full-state control design. 863  
negative. 25, 28  
positive. 61  
of state variables. 882, 884, 931
- Feedback control system, and disturbance signals. 264–269
- feedback function.** 144, 145–146, 1075
- Feedback signal.** A measure of the output of the system used for feedback to control the system. 25, 70, 143
- Feedback systems, history of. 27
- Field current controlled motor. 93
- Final value.** The value that the output achieves after all the transient constituents of the response have faded. Also referred to as the steady-state value. 84, 181  
of response of  $y(t)$ . 84
- Final value theorem.** The theorem that states that  $\lim_{t \rightarrow \infty} y(t) = \lim_{s \rightarrow 0} sY(s)$ , where  $Y(s)$  is the Laplace transform of  $y(t)$ , 84, 181
- Flow graph. *See* Signal-flow graph
- Fluid flow modeling. 116–126
- Flyball governor.** A mechanical device for controlling the speed of a steam engine. 27–28, 70
- Fly-by-wire aircraft control surface. 1033–1039
- Forward rectangular integration.** A computational method of approximating the integration of a function given by  $x(kT) \approx x((k-1)T) + T\dot{x}((k-1)T)$ , where  $t = kT$ ,  $T$  is the sample time, and  $k = 1, 2, \dots$ . 1030, 1059
- Fourier transform.** The transformation of a function of time  $f(t)$  into the frequency domain. 578, 655
- Fourier transform pair.** A pair of functions, one in the time domain, denoted by  $f(t)$ , and the other in the frequency domain, denoted by  $F(\omega)$ , related by the Fourier transform as  $F(\omega) = \mathcal{F}\{f(t)\}$ , where  $\mathcal{F}$  denotes the Fourier transform. 577–578, 655
- Frequency response.** The steady-state response of a system to a sinusoidal input signal. 576, 655  
closed-loop. 683  
measurements. 599–601  
plots. 578–583  
using control design software. 618
- Full-state feedback control law.** A control law of the form  $\mathbf{u} = -\mathbf{K}\mathbf{x}$  where  $\mathbf{x}$  is the state of the system assumed known at all times. 857, 931
- Fundamental matrix. *See* Transition matrix
- Future evolution of control systems. 49–50
- Gain margin.** The increase in the system gain when phase =  $-180^\circ$  that will result in a marginally stable system with intersection of the  $-1 + j0$  point on the Nyquist diagram. 677, 715–716, 725, 764
- Gamma-Ray Imaging Device (GRID). 1003
- Gear train. 100
- Global Positioning System (GPS). 30–31
- Graphical evaluation of residues. 83
- Graphics in MATLAB. 1060, 1068–1071
- Gravity gradient torque. 216
- Green engineering. 47  
applications of. 48–49  
principles of. 47
- Gun controllers. 30
- Gyroscope. 247
- Halo orbit. 928
- Hand, robotic. 34, 37, 66
- Helicopter control. 552, 560
- High-fidelity simulations. 123
- History of automatic control. 27
- Home appliances. 47
- Homogeneity.** The property of a linear system in which the system response,  $y(t)$ , to an input  $u(t)$  leads to the response  $\beta y(t)$  when the input is  $\beta u(t)$ . 77–78, 181
- Hot ingot robot mechanism. 703–713
- Hubble telescope. 364, 365–368
- Hybrid fuel automobile.** An automobile that uses a conventional internal combustion engine in combination with an energy storage device to provide a propulsion system. 44, 70
- Hydraulic actuator. 96, 97, 99, 166–167, 916
- IAE. 353
- Impulse signal. 328
- Index of performance. 352–361, 406, 883

- Inner product, matrix, 1066
- Input feedforward canonical form.** A canonical form described by  $n$  feedback loops involving the  $a_n$  coefficients of the  $n$ th order denominator polynomial of the transfer function and feed forward loops obtained by feeding forward the input signal, 200–201, 254
- Input signals, 327–328
- Instability.** An attribute of a system that describes a tendency of the system to depart from the equilibrium condition when initially displaced, 253, 275, 325  
in cost of feedback, 275
- Insulin delivery control system, 50, 53–54
- Insulin injections, 391
- Integral of absolute magnitude of the error, 353
- Integral of square of error, 352
- Integral of time multiplied by absolute error, 353  
optimum coefficient of  $T(s)$ , 356–357, 361
- Integral of time multiplied by error squared, 353
- Integral operator, 82
- Integrating filter, 98
- Integration network.** A network that acts in part, like an integrator, 772, 787, 855
- Intelligent vehicle/highway systems (IVHS), 527
- Internal model design.** A method of tracking reference inputs with guaranteed steady-state tracking errors, 881, 891–894, 931
- Internal model principle.** The principle that states that if  $G_c(s)G(s)$  contains the input  $R(s)$ , then the output  $y(t)$  will track  $R(s)$  asymptotically (in the steady-state) and the tracking is robust, 893, 954, 1004
- Internal Revenue Service, 38
- Inverse Laplace transform.** A transformation of a function  $F(s)$  from the complex frequency domain into the time domain, yielding  $f(t)$ , 80, 82, 84–85, 182
- Inverted pendulum, 208–209, 866–868, 875, 878, 922, 924
- ISE, 352, 396
- ITAE, 353  
optimum coefficient of  $T(s)$ , 356–357, 361
- ITSE, 353
- Jordan canonical form.** A block diagonal canonical form for systems that do not possess distinct system poles, 205, 255
- Kalman state-space decomposition.** A partition of the state space that illuminates the states that are controllable and unobservable, uncontrollable and unobservable, controllable and observable, and uncontrollable and observable, 858, 861, 931
- Kirchhoff voltage laws, 186
- Laboratory robot, 113, 131–133
- Lag network. *See* Phase-lag network
- Laplace transform.** A transformation of a function  $f(t)$  from the time domain into the complex frequency domain yielding  $F(s)$ , 72, 80–87, 181, 184
- Laplace transform pair.** A pair of functions, one in the time domain, denoted by  $f(t)$ , and the other in the frequency domain, denoted by  $F(s)$ , related by the Laplace transform as  $F(s) = \mathcal{L}\{f(t)\}$ , where  $\mathcal{L}$  denotes the Laplace transform, 81, 577, 578, 655
- Laser manipulator control system, 518–519, 522–524
- Lead network. *See* Phase-lead network
- Lead-lag network.** A network with the characteristics of both a lead network and a lag network, 798, 855
- Linear approximation.** An approximate model that results in a linear relationship between the output and the input of the device, 79, 181
- Linear approximations of physical systems, 77–80
- Linear quadratic regulator.** An optimal controller designed to minimize the quadratic performance index
- $$J = \int_0^{\infty} (\mathbf{x}^T \mathbf{Q} \mathbf{x} + \mathbf{u}^T \mathbf{R} \mathbf{u}) dt,$$
- where  $\mathbf{Q}$  and  $\mathbf{R}$  are design parameters, 891, 931
- Linear system.** A system that satisfies the properties of superposition and  
homogeneity, 77–78, 181  
simplification of, 361–364, 381
- Linearized.** Made linear or placed in a linear form. Taylor series approximations are commonly employed to obtain linear models of physical systems, 72, 182
- Locus.** A path or trajectory that is traced out as a parameter is changed, 465, 573
- Logarithmic (decibel) measure.** A measure of the gain margin defined as  $20 \log_{10}(1/d)$ ,  
where  $\frac{1}{d} = \frac{1}{|L(j\omega)|}$  when the phase shift is  $-180^\circ$ , 677, 764
- Logarithmic magnitude.** The logarithm of the magnitude of the transfer function, usually expressed in units of 20 dB, thus  $20 \log_{10}|G|$ , 585–588, 604, 639–640, 655
- Logarithmic plot. *See* Bode plot
- Logarithmic sensitivity.** A measure of the sensitivity of the system performance to specific parameter changes, given by
- $$S_k^T(s) = \frac{\partial T(s)/T(s)}{\partial K/K},$$
- where  $T(s)$  is the system transfer function and  $K$  is the parameter of interest, 495, 573
- Log-magnitude–phase diagram, 678
- Loop. A closed path that originates and terminates on the same node of a signal-flow with no node being met twice along the path, 107
- Loop gain.** The ratio of the feedback signal to the controller actuating signal. For a unity feedback system we have  $L(s) = G_c(s)G(s)$ , 259
- Loop on signal-flow graph, 99
- Loss of gain.** A reduction in the amplitude of the ratio of the output signal to the input signal through a system, usually measured in decibels, 277, 325  
in cost of feedback, 275

- Low-fidelity simulations, 123  
 Low-pass filter, 113, 133–135
- lsim** function, 231, 232, 351–353, 354, 381, 929, 1041, 1075
- Lunar excursion module (LEM), 836
- M* circles, 686
- Magnetic levitation, 168, 844, 1001
- Magnetic tape transport, 554
- Manual control system, 32
- Manual PID tuning.** The process of determining the PID controller gains by trial-and-error with minimal analytic analysis, 505, 573
- Mapping of contours in the *s*-plane, 658
- Margin, gain, 677, 715–716, 725, 764  
 phase, 678, 682, 715–716, 725, 764, 1025–1026
- margin** function, 714, 854, 1075
- Marginally stable.** A system is marginally stable if and only if the zero input response remains bounded as  $t \rightarrow \infty$ , 412, 464
- Mars rover vehicle, 276, 279–281, 461, 566, 1001
- Mason, 106
- Mason loop rule.** A rule that enables the user to obtain a transfer function by tracing paths and loops within a system, 157, 182
- Mason's signal-flow gain formula, 100, 108, 112, 152, 166, 195, 211
- Mathematical models.** Descriptions of the behavior of a system using mathematics, 72, 182
- Mathematical models of systems, 71–152
- MATLAB.** 1060  
 basics, 1060–1077  
 Bode plot, 618  
 as case sensitive, 1062  
 colon notation, 1068  
 control system characteristics, 290  
 double precision, 1064  
 functions, 1075–1076  
 graph display, 1069  
 graphics, 1060, 1068–1071  
 mathematical functions, 1062  
 matrices, 1060, 1065–1068  
 plots, 1068  
 scripts, 1060, 1071–1076  
 simulation of systems, 135–136  
 state variables and, 228
- statements and variables, 1060–1064  
 symbols, 1074  
 system performance and, 378–382  
 toolboxes, 1060
- Matrices for MATLAB, 1066–1067
- Matrix exponential function.** An important matrix function, defined as  $e^{At} = \mathbf{I} + At + (At)^2/2! + \dots + (At)^k/k! + \dots$  that plays a role in the solution of linear constant coefficient differential equations, 189, 255
- Matrix laboratory, 1065
- Maximum overshoot, 332
- Maximum power point tracking (MPPT), 113
- Maximum value of the frequency response.** A pair of complex poles will result in a maximum value for the frequency response occurring at the resonant frequency, 589, 601, 655
- Maxwell, J. C., 28, 31
- Mean arterial pressure (MAP), 282, 283
- Measurement noise.** An unwanted input signal that affects the measured output signal, 25, 70
- Measurement noise attenuation,** 268–269
- Mechanical accelerometer, 128–131
- Mechatronics.** The synergistic integration of mechanical, electrical, and computer systems, 43–47, 70
- Metallurgical industry, 36
- m-files, 1060, 1071
- Microcomputer.** A small personal computer (PC) based on a microprocessor, 1007, 1059
- Microelectromechanical systems (MEMS), 44
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- Minimum phase transfer function.** All the zeros of a transfer function lie in the left-hand side of the *s*-plane, 593, 655
- Minorsky, N., 158
- Milling machine control system, 812–818
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- Model of, DC motor, 92  
 epidemic disease, 206–207, 425–426  
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- Multiloop reduction, 146–148
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- Multivariable control system.** A system with more than one input variable or more than one output variable, 26, 70
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- Natural frequency.** The frequency of natural oscillation that would occur for two complex poles if the damping were equal to zero, 84, 182, 613, 655
- Necessary condition.** A condition or statement that must be satisfied to achieve a desired effect or result. For example, for a linear system it is necessary that the input  $u_1(t) + u_2(t)$  results in the response  $y_1(t) + y_2(t)$ , where the input  $u_1(t)$  results in the response  $y_1(t)$  and the input  $u_2(t)$  results in the response  $y_2(t)$ , 77, 182
- Negative feedback.** An output signal fed back so that it subtracts from the input signal, 25, 70
- Negative gain root locus.** The root locus for negative values of the parameter of interest, where  $-\infty < K \leq 0$ , 514–518, 573
- ngrid** function, 714, 717, 1076

- Nichols chart.** A chart displaying the curves for the relationship between the open-loop and closed-loop frequency response. 686-690, 714, 717-719, 725, 764, 974
- nichols function.** 714, 717, 1076
- Node.** The input and output points or junctions in a signal-flow graph. 107
- Nodes of signal flow graph. 107
- Noise. 258-260, 264-269, 275, 283, 284, 285, 300, 317-319
- Nomenclature. 75
- Nonminimum phase transfer functions.** Transfer functions with zeros in the right-hand  $s$ -plane. 592, 595-596, 655
- Nontouching.** Two loops in a signal-flow graph that do not have a common node. 107
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- Nonunity feedback systems. 349-352
- Nuclear reactor controls. 61, 245
- Number of separate loci.** Equal to the number of poles of the transfer function assuming that the number of poles is greater than the number of zeros of the transfer function. 473, 573
- Numerical experiments. 123
- Nyquist, H. 657
- Nyquist contour. 664
- Nyquist criterion. 664-675, 690, 725
- nyquist function. 714, 1076
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- Observability. 857-863
- Observability matrix.** A linear system is (completely) observable if and only if the observability matrix  $P_o = [C^T (CA)^T (CA^2)^T \dots (CA^{n-1})^T]^T$  has full rank, where  $A$  is an  $n \times n$  matrix. For single-input, single-output linear systems, the system is observable if and only if the determinant of the  $n \times n$  observability matrix  $P_o$  is nonzero. 861, 931
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 Low-pass filter, 113, 133–135  
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 MATLAB, 1060  
   basics, 1060–1077  
   Bode plot, 618  
   as case sensitive, 1062  
   colon notation, 1068  
   control system characteristics, 290  
   double precision, 1064  
   functions, 1075–1076  
   graph display, 1069  
   graphics, 1060, 1068–1071  
   mathematical functions, 1062  
   matrices, 1060, 1065–1068  
   plots, 1068  
   scripts, 1060, 1071–1076  
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   state variables and, 228  
   statements and variables, 1060–1064  
   symbols, 1074  
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- Phase variables.** The state variables associated with the phase variable canonical form, 197, 255
- Phase-lag compensation.** A widely-used compensator that possesses one zero and one pole with the pole closer to the origin of the  $s$ -plane. This compensator reduces the steady-state tracking errors, 772, 855
- Phase-lag network.** A network that provides a negative phase angle and a significant attenuation over the frequency range of interest, 772–773, 855
- Phase-lead compensation.** A widely-used compensator that possesses one zero and one pole with the zero closer to the origin of the  $s$ -plane. This compensator increases the system bandwidth and improves the dynamic response, 768–771, 827, 855
- Phase-lead network.** A network that provides a positive phase angle over the frequency range of interest. Thus, phase lead can be used to cause a system to have an adequate phase margin, 769, 855
- Photovoltaic generators, 113–115, 605–607
- Physical state variables, 186–187
- Physical variables.** The state variables representing the physical variables of the system, 204–205, 255
- PI controller. *See* Proportional plus integral (PI) controller
- PID controller.** A widely used controller used in industry of the form
- $$G_c(s) = K_p + \frac{K_I}{s} + K_D s,$$
- where  $K_p$  is proportional gain,  $K_I$  is the integral gain, and  $K_D$  is the derivative gain, 285, 286, 287, 289, 502–514, 573
- design of robust, 948–954, 1004–1005
- in discrete-time,
- $$G_c(z) = K_1 + \frac{K_2 T s}{z-1} + K_3 \frac{z-1}{T z},$$
- 1031, 1059
- in frequency domain, 713–714
- of wind turbines for clean energy, 696–699
- PID tuning.** The process of determining the PID controller gains, 505, 573
- Plant. *See* Process
- Plastic extrusion, 1057
- Plotting using MATLAB, 149, 1068, 1076
- Pneumatica*, 27
- Polar plot.** A plot of the real part of  $G(j\omega)$  versus the imaginary part of  $G(j\omega)$ , 579, 655
- Pole placement.** A design methodology wherein the objective is to place the eigenvalues of the closed-loop system in desired regions of the complex plane, 858, 931
- Poles.** The roots of the denominator polynomial (i.e., the roots of the characteristic equation) of the transfer function, 82–83, 182
- Pole-zero map, 139, 140–141
- Political feedback model, 38
- poly** function, 136, 441, 928, 1076
- polyval** function, 136, 1076
- Polzunov, L., 27
- Pontryagin, L. S., 30
- Position error constant  $K_p$ .** The constant evaluated as  $\lim_{s \rightarrow 0} G_c(s)G(s)$ . The steady-state error for a step input (of magnitude  $A$ ) is equal to  $A/(1 + K_p)$ , 345, 406
- Positive feedback.** An output signal fed back so that it adds to the input signal, 61–62, 70
- Positive feedback loop.** A feedback loop wherein the output signal fed back so that it adds to the input signal, 105
- Potentiometer, 100
- Power flow, 52
- Power plants, 36
- Power quality monitoring (green engineering), 48
- Precision.** The degree of exactness or discrimination with which a quantity is stated, 1011, 1059
- Precision speed control system, 555
- Prefilter.** A transfer function  $G_p(s)$  that filters the input signal  $R(s)$  prior to calculating the error signal, 800–803, 855, 1005
- Principle of superposition.** The law that states that if two inputs are scaled and summed and routed through a linear, time-invariant system, then the output will be identical to the sum of outputs due to the individual scaled inputs when routed through the same system, 77, 182
- Principle of the argument.** *See* Cauchy's theorem
- Printer belt drive, 222–228
- Process.** The device, plant, or system under control, 24, 70
- Process controller. *See* PID controller
- Productivity.** The ratio of physical output to physical input of an industrial process, 29, 70
- Proportional plus derivative (PD) controller.** A two-term controller of the form  $G_c(s) = K_p + K_D s$ , where  $K_p$  is the proportional gain and  $K_D$  is the derivative gain, 503, 574, 855
- Proportional plus integral (PI) controller.** A two-term controller of the form  $G_c(s) = K_p + \frac{K_I}{s}$ , where  $K_p$  is the proportional gain and  $K_I$  is the integral gain, 503, 574, 787, 855
- Pseudo-quantitative feedback system, 974–975
- pzmap** function, 136, 139, 163, 1076
- Quantitative feedback theory (QFT), 974
- Quarter amplitude decay.** The amplitude of the closed loop response is reduced approximately to one-fourth of the maximum value in one oscillatory period, 505, 574

- Rack and pinion, 97, 101
- Radio-based navigation system, 30–31
- Ramp input, optimum coefficients of  $T(s)$ , 361
- steady-state error, 346
- test signal equation, 328
- Reaction curve.** The response obtained by taking the controller off-line and introducing a step input. The underlying process is assumed to be a first-order system with a transport delay, 509
- Reduced sensitivity, 261
- Reference input.** The input to a control system often representing the desired output, denoted by  $R(s)$ , 143, 182, 879–881
- Regulator problem, 864
- Regulatory bodies, 37
- Relative stability.** The property that is measured by the relative real part of each root or pair of roots of the characteristic equation, 409, 421, 464
- by the Nyquist criterion, 675–682
- by the Routh-Hurwitz criterion, 421
- Remote manipulators, 247, 839
- Remotely operated vehicle, 700–703, 720–722
- Residues.** The constants  $k_j$  associated with the partial fraction expansion of the output  $Y(s)$  when the output is written in a residue-pole format, 83, 85, 86, 182
- Resonant frequency.** The frequency,  $\omega_r$ , at which the maximum value of the frequency response of a complex pair of poles is attained, 588–589, 655
- Rise time.** The time for a system to respond to a step input and attain a response equal to a percentage of the magnitude of the input. The 0–100% rise time,  $T_r$ , measures the time to 100% of the magnitude of the input. Alternatively,  $T_{r1}$  measures the time from 10% to 90% of the response to the step input, 332, 406–407
- Risk.** Uncertainties embodied in the unintended consequences of a design, 39, 40, 70
- Robot.** Programmable computers integrated with a manipulator. A reprogrammable, multifunctional manipulator used for a variety of tasks, 33–34, 70
- controlled motorcycle, 428–434
- design of laboratory, 113, 131–133
- mobile, steering control, 380–381
- replication, 524–527
- Robot control system, 524–527, 942–948, 1005
- Robust control system.** A system that exhibits the desired performance in the presence of significant plant uncertainty, 932–1005
- using control design software, 975–979
- Robust PID control, 948–954
- Robust stability criterion.** A test for robustness with respect to multiplicative perturbations in which stability is guaranteed if  $|M(j\omega)| < \left| 1 + \frac{1}{G(j\omega)} \right|$ , for all  $\omega$ , where  $M(s)$  is the multiplicative perturbation, 938–939, 1005
- Roll-wrapping machine (RWM), 980, 991
- Root contours.** The family of loci that depict the effect of varying two parameters on the roots of the characteristic equation, 494, 574
- Root locus.** The locus or path of the roots traced out on the  $s$ -plane as a parameter is changed, 466–470, 574, 725, 1026–1030
- angle of departure, 480
- asymptote, 473
- breakaway point, 476
- concept, 466–470
- of digital control systems, 1026–1030
- plot obtaining, 533–537
- sensitivity and, 495–502, 538
- steps in sketching, 482
- using control design software, 532–538
- in the  $z$ -plane, 1027–1028
- Root locus method.** The method for determining the locus of roots of the characteristic equation  $1 + K^*P(s) = 0$  as  $K$  varies from 0 to infinity, 466, 471–489, 574
- parameter design, 489–494
- Root locus segments on the real axis.** The root locus lying in a section of the real axis to the left of an odd number of poles and zeros, 472, 474, 574
- Root sensitivity.** The sensitivity of the roots as a parameter changes from its normal value. The root sensitivity is given by  $S_K^r = \frac{\partial r}{\partial K/K}$ —the incremental changes in the root divided by the proportional change of the parameter, 495, 574
- to parameters. A measure of the sensitivity of the roots (i.e., the poles and zeros) of the system to changes in a parameter defined by  $S_\alpha^r = \frac{\partial r_i}{\partial \alpha/\alpha}$  where  $\alpha$  is the parameter and  $r_i$  is the root, 934, 1005
- roots function,** 136, 436, 440, 441, 1076
- Rotating disk speed control, 52–53
- Rotor wind system, 805–809, 818–824
- Routh-Hurwitz criterion.** A criterion for determining the stability of a system by examining the characteristic equation of the transfer function. The criterion states that the number of roots of the characteristic equation with positive real parts is equal to the number of changes of sign of the coefficients in the first column of the Routh array, 413–421, 426, 435–437, 464
- Routh-Hurwitz stability, 408
- R.U.R. (play), 34
- Sampled data.** Data obtained for the system variables only at discrete intervals. Data obtained once every sampling period, 1009, 1059
- Sampled-data system.** A system where part of the system acts on sampled data (sampled variables), 1009–1012, 1059
- Sampling period.** The period when all the numbers leave or enter the computer. The period for which the sampled variable is held constant, 1009, 1059
- Scanning tunneling microscope (STM), 997

- Scripts, 1060, 1071–1076  
 comments, 1072  
 defined, 1071  
 header, 1072  
 invoking, 1071  
 TeX characters use of, 1072–1073
- Second order system response,  
 effect of third pole and zero,  
 336–342
- Second-order system,  
 performance of, 330–336
- Self-balancing scale, 485–489
- Self-healing process, 52
- Semiconductors, 35
- Sensitivity. *See also* System  
 sensitivity  
 of control systems to parameter  
 variations, 261–264  
 of root control systems, 496  
 root locus and, 495–502, 538
- Sensitivity function.** The function  
 $S(s) = [1 + G_c(s)G(s)]^{-1}$  that  
 satisfies the relationship  
 $S(s) + T(s) = 1$ , where  $T(s)$  is  
 the complementary sensitivity  
 function, 260, 265, 268, 287, 300,  
 938, 1005
- Separation principle.** The principle  
 that states that the full-state feed-  
 back law and the observer can be  
 designed independently and when  
 connected will function as an  
 integrated control system in the  
 desired manner (*i.e.*, stable),  
 863, 874, 931
- Sequential design example, 54–56,  
 150–152, 231–235, 295–299,  
 382–386, 443–446, 538–540,  
 624–625, 722–725, 824–826,  
 910–912, 980–982, 1045–1047
- Series connection, 142–145
- series function.** 136, 142, 145,  
 146, 1076
- Settling time.** The time required for  
 the system output to settle within  
 a certain percentage of the input  
 amplitude, 333, 407
- Ship stabilization, 309, 837–838
- Signal-flow graph.** A diagram that  
 consists of nodes connected by  
 several directed branches and  
 that is a graphical representation  
 of a set of linear relations,  
 106–112, 182  
 block diagram models and,  
 193–204  
 models, 106
- Simplification of linear systems,  
 361–364
- Simulation.** A model of a system  
 that is used to investigate the  
 behavior of a system by utilizing  
 actual input signals, 123,  
 135–149, 182
- Smart grid  
 control systems, 50–52  
 definition, 47, 50
- Smart meters, 50
- Social feedback model, 38
- Solar cells, 113
- Solar energy (green engineering), 48
- Space shuttle, 643–644, 744–746,  
 1051–1052
- Space station, 215–221
- Space telescope, 957–960
- Spacecraft, 160, 163, 215–221
- Specifications.** Statements that  
 explicitly state what the  
 device or product is to be  
 and is to do. A set of prescribed  
 performance criteria, 39, 70
- Speed control system, 265–267,  
 270–272, 290–292, 314,  
 318, 319  
 for automobiles, 311  
 for power generator, 553  
 for steel rolling mill, 265
- s-plane.** The complex plane where,  
 given the complex number  
 $s = \sigma + j\omega$ , the  $x$ -axis (or hori-  
 zontal axis) is the  $\sigma$ -axis, and the  
 $y$ -axis (or vertical axis) is the  
 $j\omega$ -axis, 82, 182
- Spring-mass-damper system,  
 136–140
- Stability.** A performance measure of  
 a system. A system is stable if all  
 the poles of the transfer function  
 have negative real parts,  
 409, 464  
 in frequency domain, 656–764  
 of linear feedback systems,  
 408–464  
 of state variable systems, 423–426  
 for unstable process, 441–443  
 using Nyquist criterion, 664  
 using Routh–Hurwitz criterion,  
 413–421, 426, 435–437
- Stability of a sampled-data system.**  
 The stable condition exists when  
 all the poles of the closed-loop  
 transfer function  $T(z)$  are within  
 the unit circle on the  
 $z$ -plane, 1059
- Stabilizable.** A system in which  
 the states that are not  
 controllable are naturally  
 stable, 858, 931
- Stabilizing controller.** A controller  
 that stabilizes the closed-loop  
 system, 875, 931
- Stable system.** A dynamic system  
 with a bounded system  
 response to a bounded input,  
 409, 464
- State differential equation.** The dif-  
 ferential equation for the state  
 vector:  $\dot{\mathbf{x}} = \mathbf{Ax} + \mathbf{Bu}$ , 188–193,  
 255
- State of a system.** A set of numbers  
 such that the knowledge of these  
 numbers and the input function  
 will, with the equations describing  
 the dynamics, provide the future  
 state of the system, 184–187, 255
- State transition matrix,  $\Phi(t)$ .** The  
 matrix exponential function that  
 describes the unforced response  
 of the system, 190
- State variable feedback.** The use of  
 control signal formed as a  
 direct function of all the state  
 variables, 248, 277, 882, 884, 931
- State variable system design using  
 control design software, 904–910
- State variables.** The set of  
 variables that describe the  
 system, 184–254, 255  
 of dynamic system, 184–187
- State vector.** The vector matrix  
 containing all  $n$  state variables,  
 $x_1, x_2, \dots, x_n$ , 188, 255
- Statements and variables,  
 MATLAB, 1060–1064
- State-space representation.** A time-  
 domain model comprised of the  
 state differential equation,  
 $\dot{\mathbf{x}} = \mathbf{Ax} + \mathbf{Bu}$ , and the output  
 equation,  $\mathbf{y} = \mathbf{Cx} + \mathbf{Du}$ , 189,  
 228–231, 255
- Steady state.** The value that the out-  
 put achieves after all the tran-  
 sient constituents of the response  
 have faded. Also referred to as  
 the final value, 84, 182  
 of response of  $y(t)$ , 84
- Steady-state error.** The error when  
 the time period is large and the  
 transient response has decayed,  
 leaving the continuous response,  
 272–275, 325

- of feedback control system, 344–352
- Steady-state response.** The constituent of the system response that exists a long time following any signal initiation, 327, 407
- Steel rolling mill, 36, 265, 691–693, 757, 760, 991
- Steering control system, of automobile, 32, 650  
of mobile robot, 347–350  
of ship, 748
- Step input, 344–346  
optimum coefficient of  $T(s)$ , 357  
steady-state error, 344  
test signal equation, 328
- Submarine control system, 242–243, 244–245
- Superposition, principle of, 77
- Symbols, in MATLAB, 1074  
used in book, 75
- Synthesis.** The process by which new physical configurations are created. The combining of separate elements or devices to form a coherent whole, 40, 70
- sys function, 142, 146
- System.** An interconnection of elements and devices for a desired purpose, 24, 70  
bandwidth, 690  
performance, 378–382
- System sensitivity.** The ratio of the change in the system transfer function to the change of a process transfer function (or parameter) for a small incremental change, 262, 325  
to parameters. A measure of the system sensitivity to changes in a parameter defined by  $S_a^T = \frac{\partial T/T}{\partial a/a}$  where  $a$  is the parameter and  $T$  is the system transfer function, 934, 1005
- Systems with uncertain parameters, 940–942
- Tables, of differential equations for elements, 74  
of Laplace transform pairs, 81  
through- and across-variables for physical systems, 73  
of transfer function plots, 726–733  
of transfer functions, 98–101
- Tachometer, 100
- Tacoma Narrows Bridge, 410–412
- Taylor series.** A power series defined by  $g(x) = \sum_{m=0}^{\infty} \frac{g^{(m)}(x_0)}{m!} (x - x_0)^m$ . For  $m < \infty$ , series is an approximation which is used to linearize functions and system models, 78, 182
- Test input signal.** An input signal used as a standard test of a system's ability to respond adequately, 328–330, 407
- Thermal heating system, 101
- Through-variable.** A variable that has the same value at both ends of an element, 72, 75
- Time constant.** The time interval necessary for a system to change from one state to another by a specified percentage. For a first order system, the time constant is the time it takes the output to manifest a 63.2% change due to a step input, 88, 182
- Time delay.** A time delay,  $T$ , so that events occurring at time  $t$  at one point in the system occur at another point in the system at a later time  $t + T$ , 690–695, 764
- Time domain.** The mathematical domain that incorporates the time response and the description of a system in terms of time  $t$ , 184, 255  
design, 857  
Time-domain specifications, 378–380  
Time response, by a discrete-time evaluation, 211  
and state transition matrix, 211–214
- Time-varying system.** A system for which one or more parameters may vary with time, 87, 255
- Tracked vehicle turning control, 426–428, 427–441
- Tracking error. See Error signal
- Trade-off.** The result of making a judgment about how to compromise between conflicting criteria, 23, 39, 70
- Transfer function.** The ratio of the Laplace transform of the output variable to the Laplace transform of the input variable, 87, 182  
of complex system, 112  
of DC motor, 92–96  
of dynamic elements and networks, 98–101  
of hydraulic actuator, 96–101  
of interacting system, 109–110  
of linear systems, 87  
in m-file script, 135, 136  
minimum phase and nonminimum phase, 592–593  
of multi-loop system, 111–112  
of op-amp circuit, 89–90  
from state equation, 209–211  
of system, 90–92  
table of dynamic elements and networks, 98–101
- Transfer function in the frequency domain.** The ratio of the output to the input signal where the input is a sinusoid. It is expressed as  $G(j\omega)$ , 582, 655
- Transient response.** The constituent of the system response that disappears with time, 269, 325, 327, 407  
relationship to root location, 342–344  
of second-order system, 330
- Transition matrix  $\Phi(t)$ .** The matrix exponential function that describes the unforced response of the system, 190, 255  
evaluation by signal flow graph methods, 212
- Twin lift, 64
- Twin-T network, 592
- Type number.** The number  $N$  of poles of the transfer function,  $G_c(s)G(s)$ , at the origin.  $G_c(s)G(s)$  is the loop transfer function, 345, 407
- Ultimate gain.** The PID controller proportional gain,  $K_p$ , on the border of instability when  $K_D = 0$  and  $K_I = 0$ , 509
- Ultimate period.** The period of the sustained oscillations when  $K_p$  is the ultimate gain and  $K_D = 0$  and  $K_I = 0$ , 509
- Ultra-precision diamond turning machine, 962–965
- Uncertain parameters, 940–942
- Underdamped.** The case where the damping ratio is  $\zeta < 1$ , 76, 136, 182

- Unit impulse.** A test input consisting of an impulse of infinite amplitude and zero width, and having an area of unity. The unit impulse is used to determine the impulse response, 328, 407
- Unity feedback.** A feedback control system wherein the gain of the feedback loop is one, 143, 182
- Unmanned aerial vehicles (UAVs), 38, 39, 306
- Unstable system, 409, 410
- Variables for physical systems, 73
- Vehicle traction control, 1056
- Velocity error constant,  $K_v$ .**  
The constant evaluated as  $\lim_{s \rightarrow 0} [sG_r(s)G(s)]$ . The steady-state error for a ramp input (of slope  $A$ ) for a system is equal to  $A/K_v$ , 346, 407
- Velocity input, 319
- Vertical takeoff and landing (VTOL) aircraft, 456, 743, 928
- Viscous damper.** A type of mechanical damper where the model of the friction force is linearly proportional to the velocity of the mass, 75
- Vyshnegradskii, I. A., 28
- Water clock, 27
- Water level control, 27–28, 63, 119–126, 173
- Watt, James, 27, 31
- Welding control, 420–421
- Wind energy (green engineering), 48
- Wind power, 44, 45–46
- Wind turbines, 696–699  
rotor speed control, 519–522
- Workspace, variables in, 1063
- Worktable motion control, 1031–1033
- X-Y plotter, 809–811
- Zero-order hold.** A mathematical model of a sample and data hold operation whose input–output transfer function is represented by  $G_o(s) = \frac{1 - e^{-sT}}{s}$ , 1011, 1059
- Zeros.** The roots of the numerator polynomial of the transfer function, 82–83, 182
- Ziegler-Nichols PID tuning method.** The process of determining the PID controller gains using one of several analytic methods based on open-loop and closed-loop responses to step inputs, 505, 510–513, 574
- z-plane.** The plane with the vertical axis equal to the imaginary part of  $z$  and the horizontal axis equal to the real part of  $z$ , 1059
- z-plane root locus, 1027–1028
- z-transform.** A conformal mapping from the  $s$ -plane to the  $z$ -plane by the relation  $z = e^{sT}$ . A transform from the  $s$ -domain to the  $z$ -domain, 1012–1017, 1059